



Action TU1208 Civil Engineering Applications of Ground Penetrating Radar

Final Conference

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National Institute of Telecommunications of Poland Development and testing of an improved reconfigurable step-frequency GPR

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Talk Layout

- The reconfigurable GPR system
- The implemented prototype
- Interference mitigation
- GPR results
- Conclusions





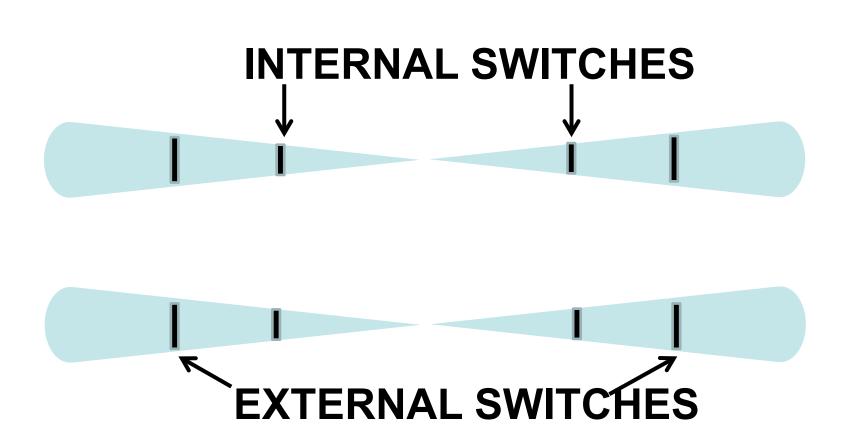
The reconfigurable GPR system

- Reconfigurable antennas
- Reconfigurable power
- Reconfigurable integration time

The reconfiguration is conceived in the spectral domain and takes into account the background medium at hand.



Reconfigurable GPR antennas





The implemented prototype www.aitechnet.com



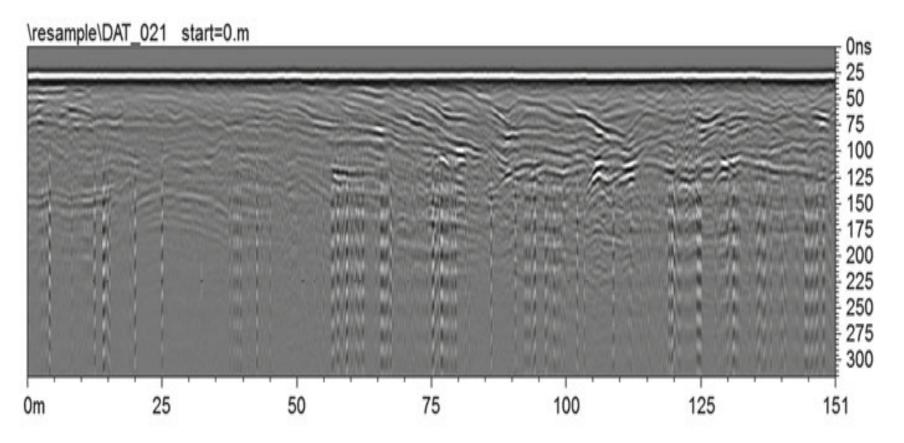
Three equivalent antennas with the same gap.

Three operation bands covering an ultra wide frequency range from 50 to 1000 MHz, with central frequency at about 120, 240 and 550 MHz.

One, two or three couples of antennas can simultaneously acquire data.



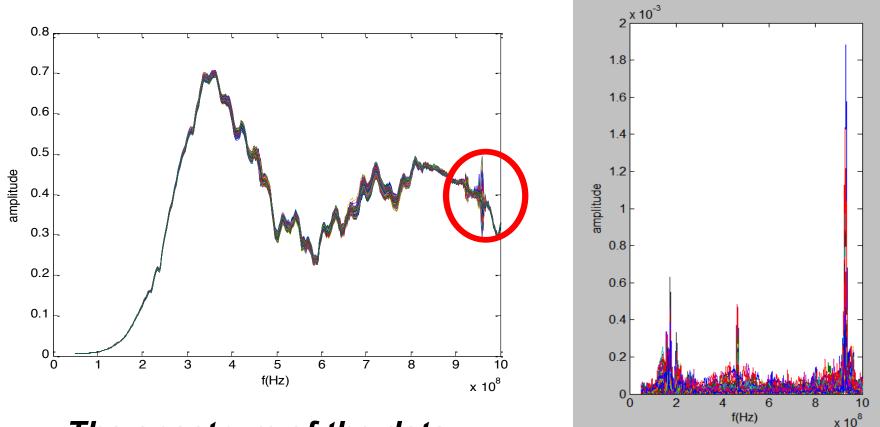
Interference mitigation



Dean Goodman and Salvatore Piro, GPR Remote Sensing in Archaeology, Springer, 2013.



How can we recognize the "interferenced" frequencies?

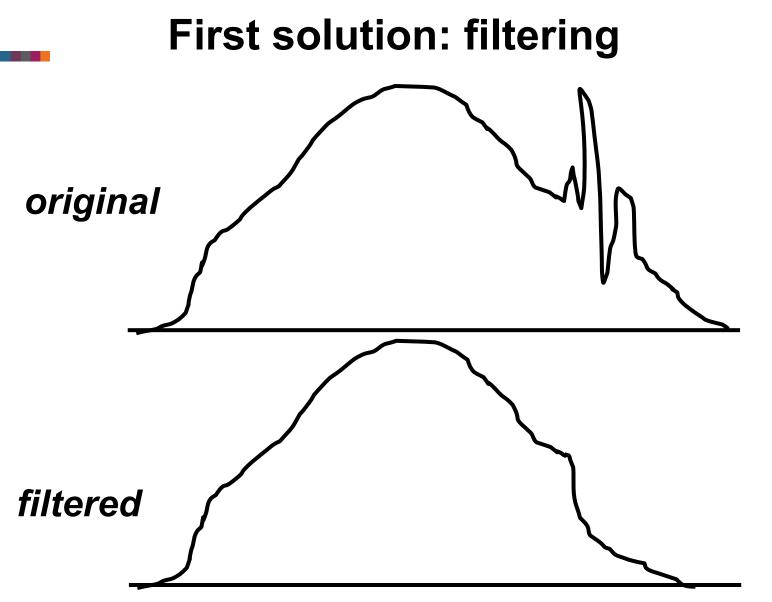


The spectrum of the data

Spectrum's slope

....too ambiguous and case driven results...





Drawbacks: loss of information and possible artifacts

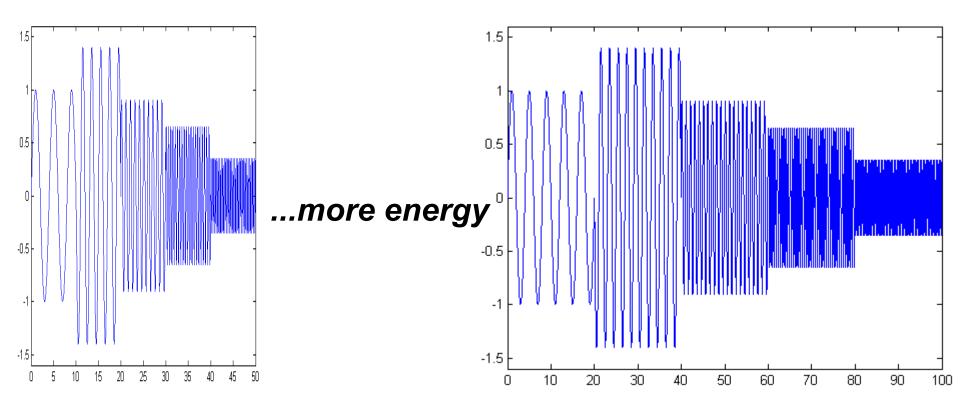
Second solution: radiating more power



Drawbacks: saturation or even damaging the receiver; illegal or even harmful operation



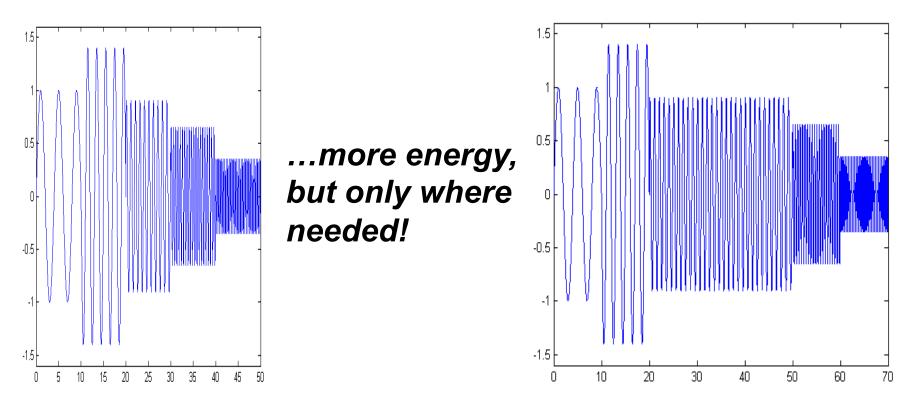
Third solution (step frequency systems): prolonging the integration time of all the harmonics



Drawbacks: the required time is likely to become quite long



Proposed solution: selective prolonging of the most "disturbed" harmonics



Pros: No filtering, no increase of radiated power, limited prolongation of acquisition time.



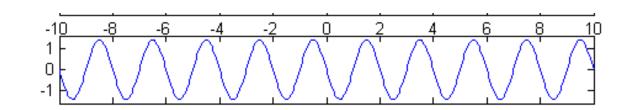
Proposed solution: selective prolonging of the most "disturbed" harmonics

Requirements:

A reconfigurable system is needed (hardware), the disturbed frequencies have to be identified, an algorithm has to be developed and implemented (software)



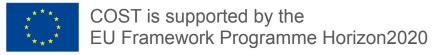
Identification of the interference from the data: retrieving *I* and *Q* components



$$A\cos(2\pi ft + \phi) = A\cos(\phi)\cos(2\pi ft) - A\sin(\phi)\sin(2\pi ft) =$$

= $I\cos(2\pi ft) + Q\sin(2\pi ft)$
 $I = A\cos(\phi)$ $Q = -A\sin(\phi)$

I and Q are the in-phase and in-quadrature components of the received harmonic and are extracted from the received harmonic signal, knowing the transmitted one.

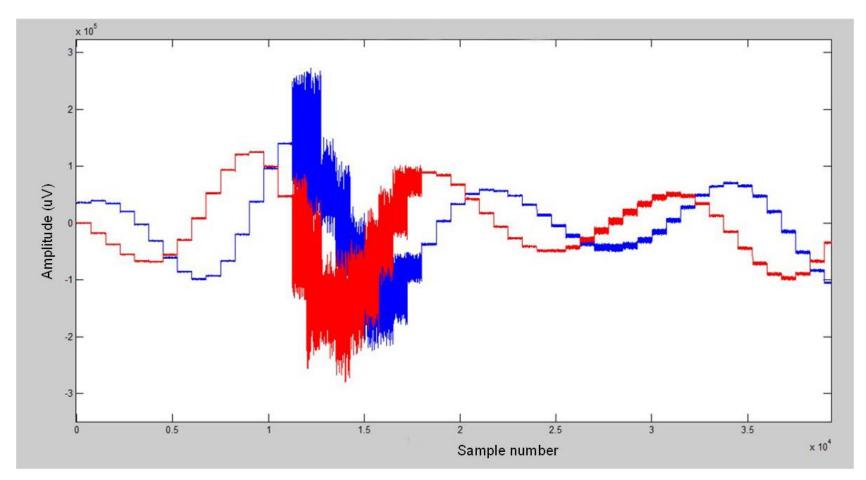


Averaging on N in-phase and in-quadrature samples

$$I_{m} = \frac{I_{1} + I_{2} + I_{3} + \dots + I_{N}}{N}$$
$$Q_{m} = \frac{Q_{1} + Q_{2} + Q_{3} + \dots + Q_{N}}{N}$$

The praxis for <u>any</u> stepped frequency system is to measure *N* consecutive times the *I* and *Q* components and retain the average (or medium) value.

Representation of the *I* (red curve) and Q (blue curve) samples frequency by frequency in an experimental case





The Variance of the samples

 $\begin{cases} \sigma_I^2 = \frac{I_1^2 + I_2^2 + \dots I_N^2}{N} - \left(\frac{I_1 + I_2 + \dots I_N}{N}\right)^2 \\ \sigma_Q^2 = \frac{Q_1^2 + Q_2^2 + \dots Q_N^2}{N} - \left(\frac{Q_1 + Q_2 + \dots Q_N}{N}\right)^2 \end{cases}$

The Matrix of variance

$$MI(k,h) = \sigma_I^2(f_k,tr_h) + \sigma_Q^2(f_k,tr_h)$$

The Index of Interference

$$VI(k) = \max_{h} MI(k,h)$$

The enlargement factor (= 1 for M=1)

$$W_k = \min\left[10, Ceil\left(M\frac{VI(k)}{\max(VI)}\right)\right]$$

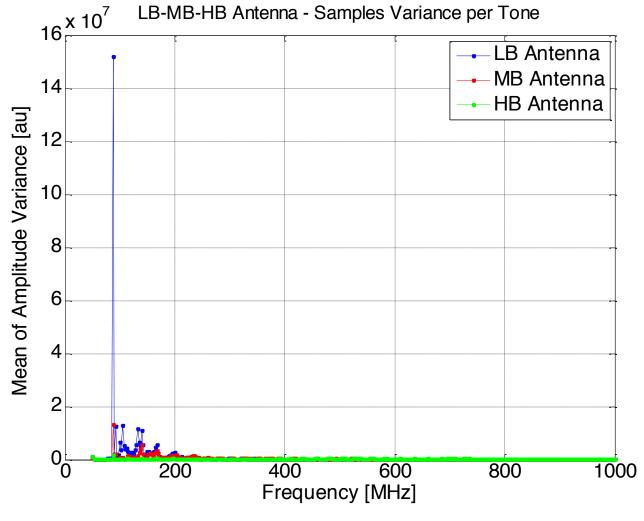


Reconfiguration "Protocol"

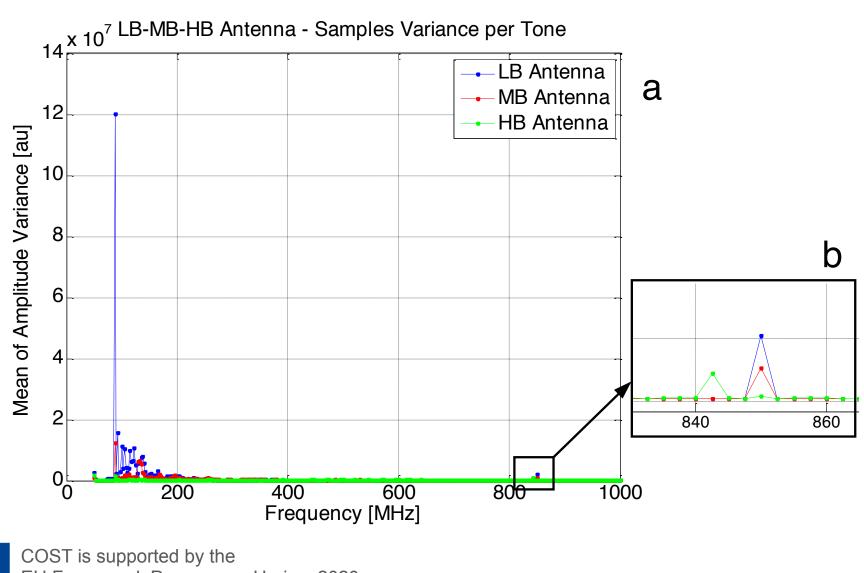
- Gather a calibration B- Scan
- Evaluate the interference index (for each couple of antennas) and the B-Scan
- Set optionally an integer number M (for each couple of antennas) meaning "how many times you would like to prolong the most disturbed tone"



A preliminary experiment indoor at IBAM-CNR



The same experiment with two mobile phones calling each other



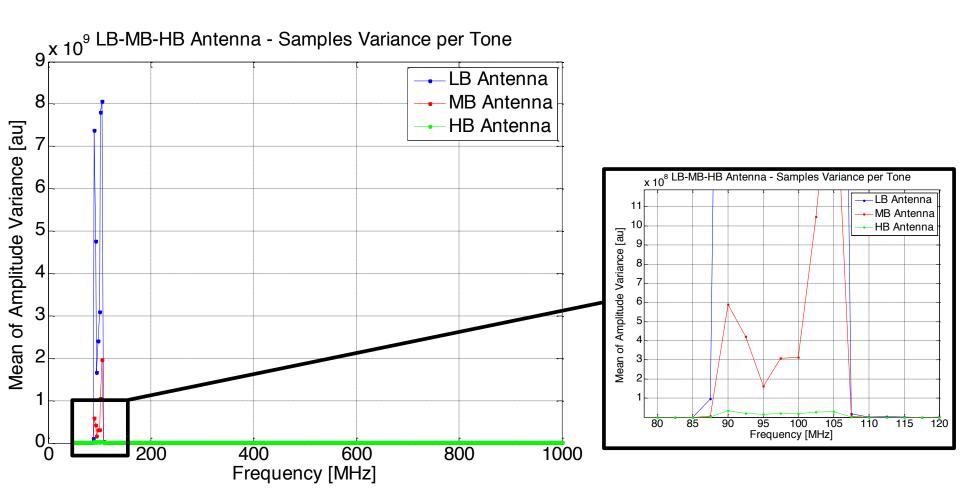
EU Framework Programme Horizon2020

Effects in a practical case





Measured Interference Index Interference from FM-broadcast radio transmissions



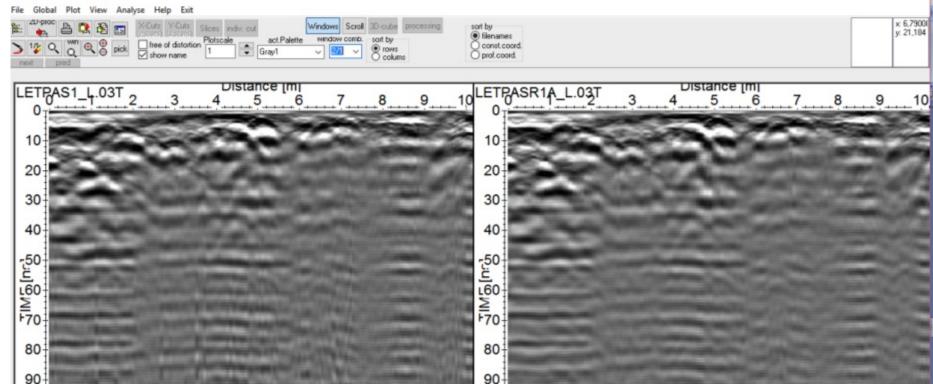
Results of our prototype

Data without reconfiguration

Data with reconfiguration

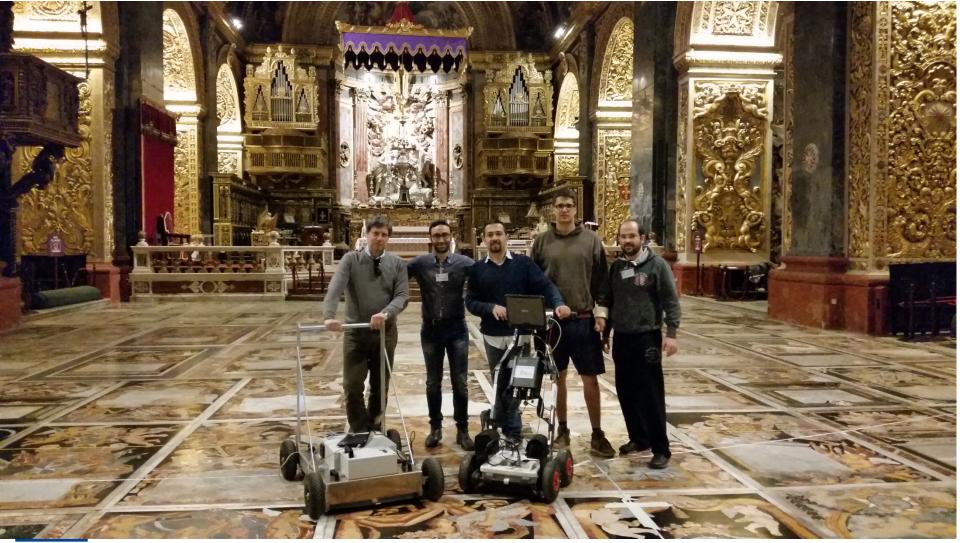
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Reflexw - 3D-datainterpretation

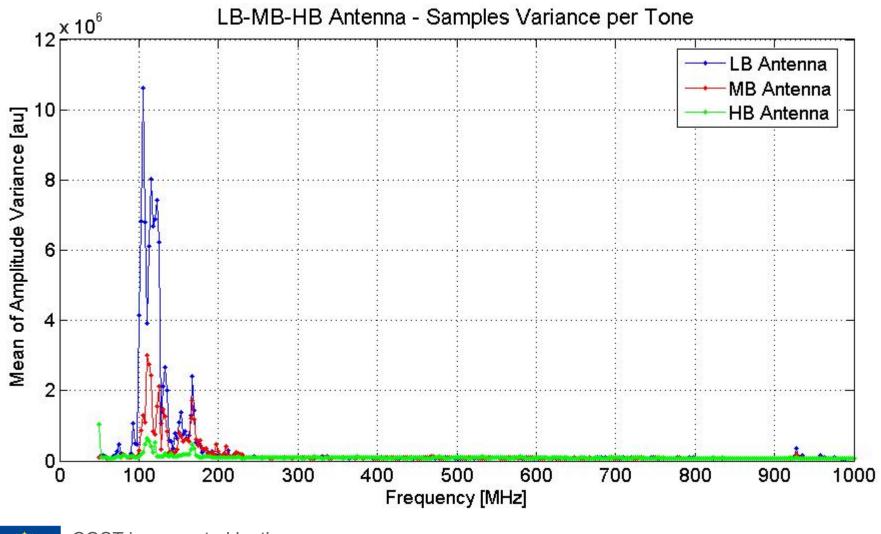




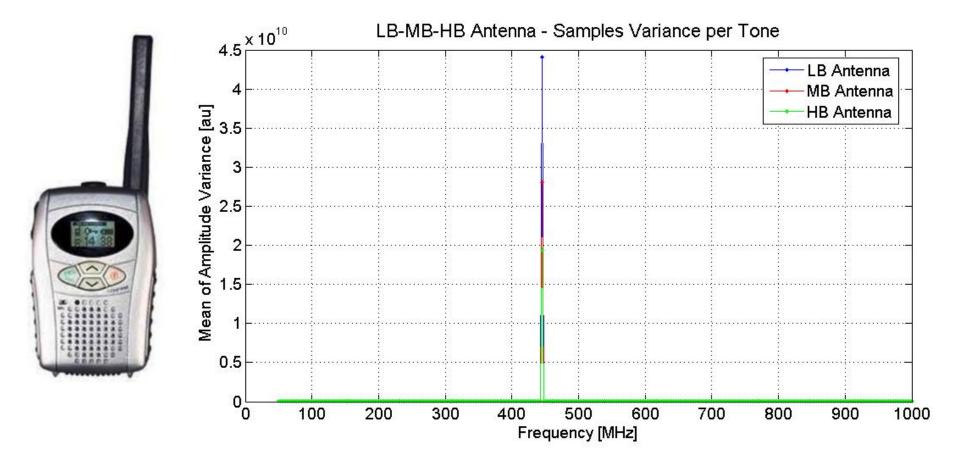
Experiments in the Chapel of Aragone, Co-cathedral of St. John in Valletta, Malta



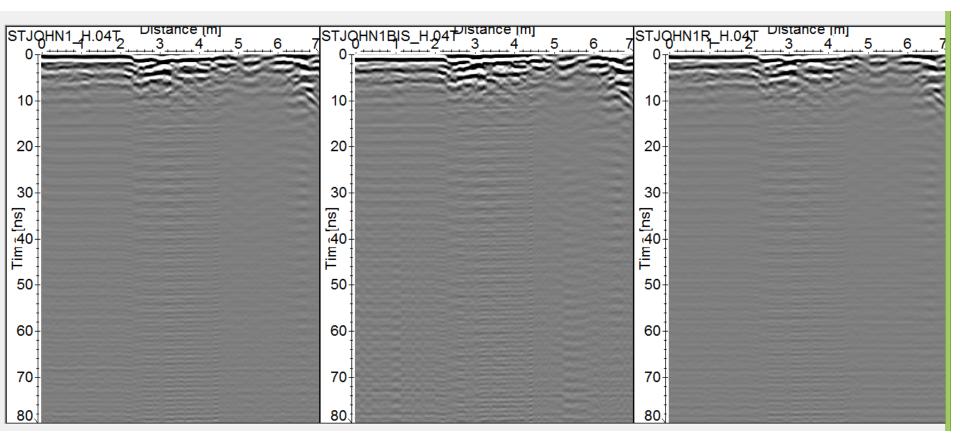
Index of interference in "standard" conditions



Index of interference with a transceiver of the staff active



Reconfiguration results

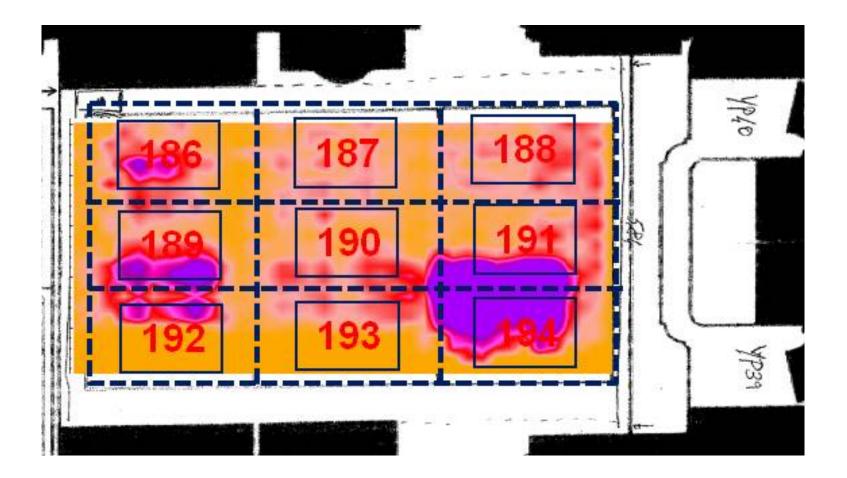


default integration times transceiver not active default integration times transceiver active

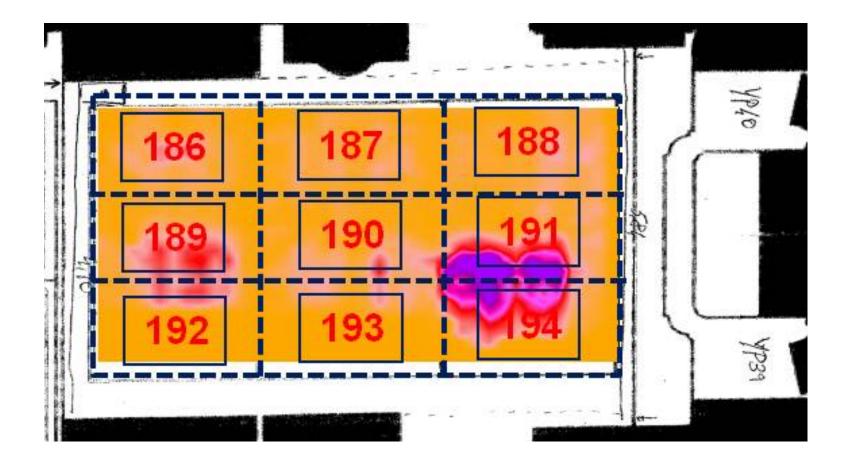
reconfigured integration times, transceiver active



Slice at about 35 cm in the chapel of Aragon



Slice at about 60 cm in the chapel of Aragon

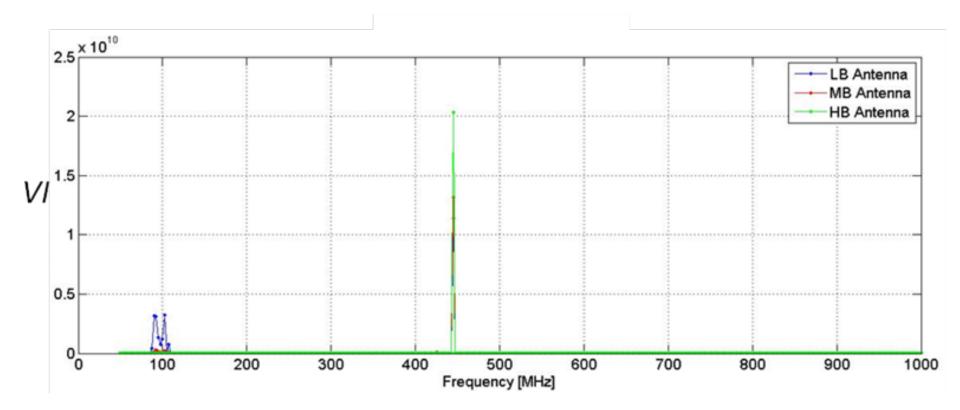


Further experiment with transceivers

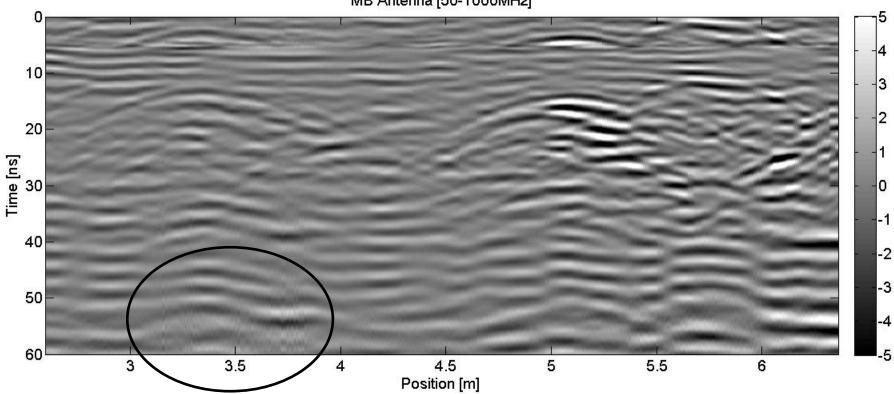




The Index of Interference



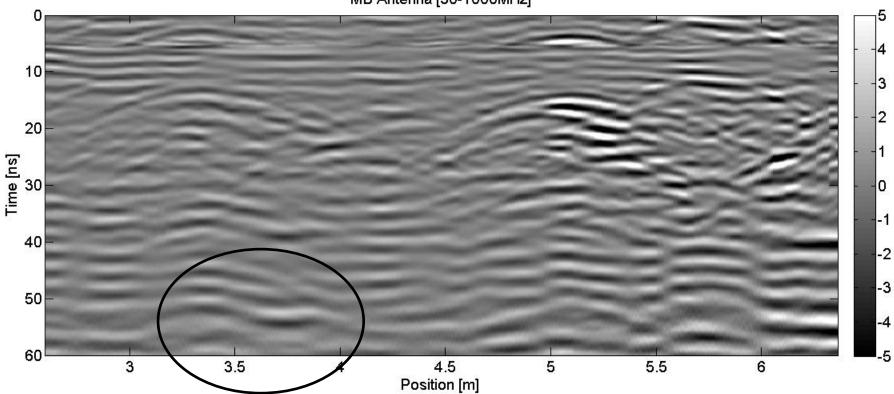
Data without reconfiguration



MB Antenna [50-1000MHz]



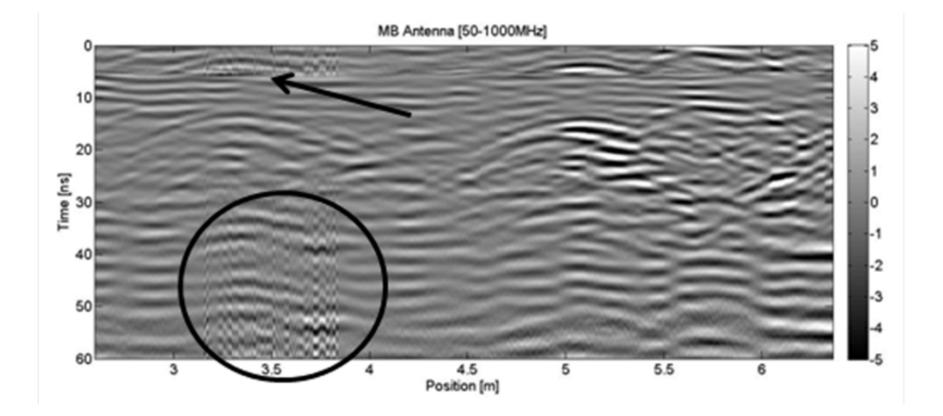
Data with reconfiguration



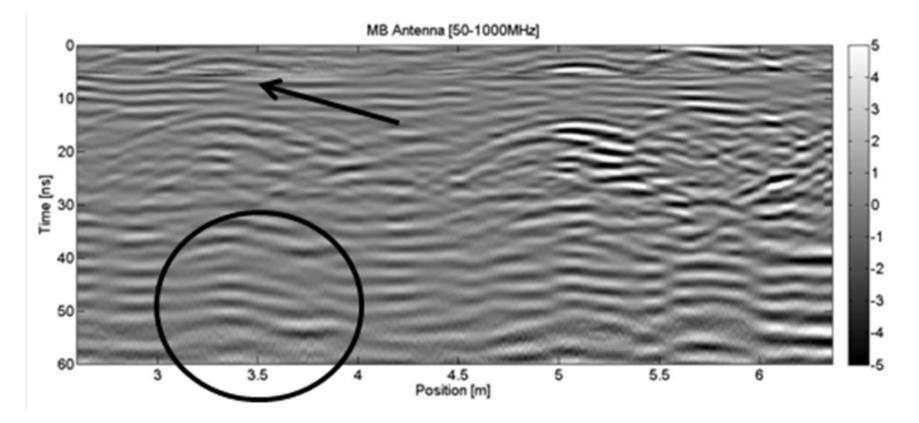
MB Antenna [50-1000MHz]



Data without reconfiguration with 10 samples instead of 63 as before



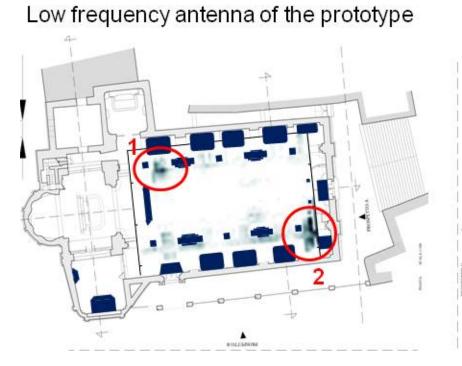
Data with reconfiguration with 10 samples instead of 63 as before



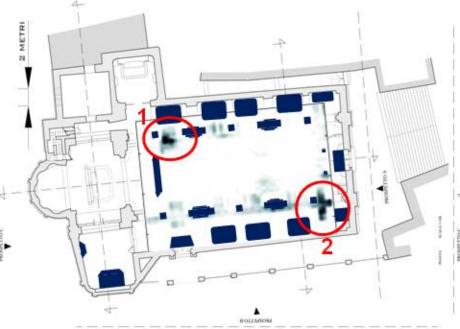


Parabita

Slice at 95cm



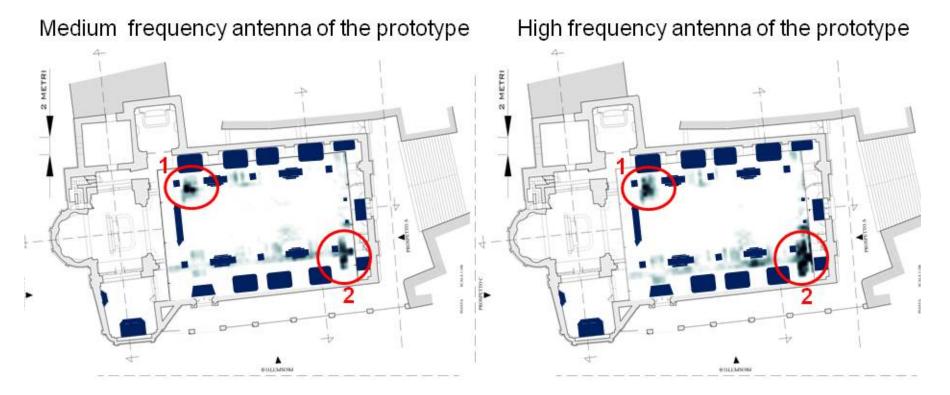
Medium frequency antenna of the prototype



.2b

Parabita

Slice at 95cm

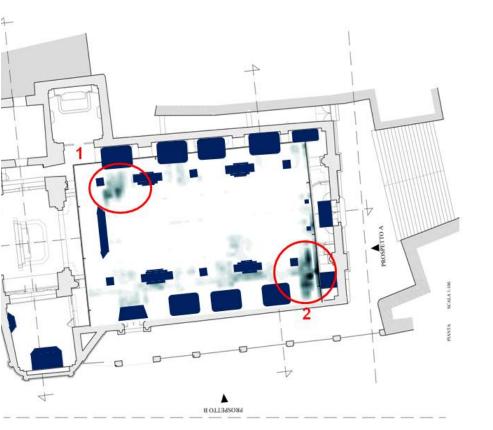


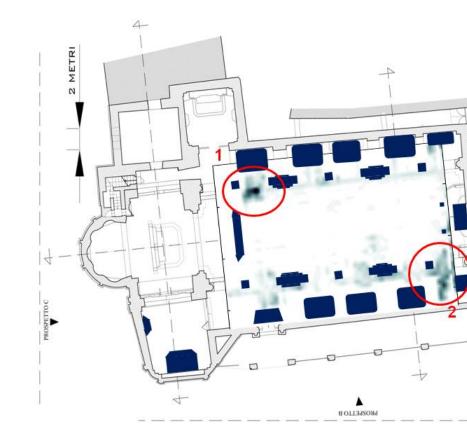
Parabita

Slice at 95cm

pulsed system antenna at 600MHz

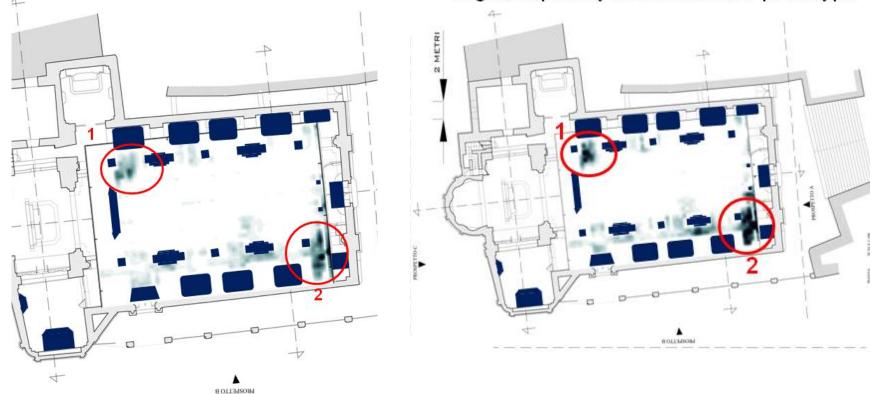
pulsed system antenna at 200MHz





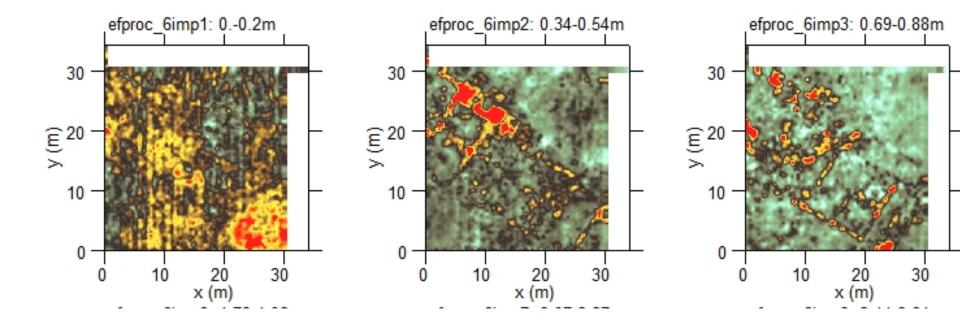


pulsed system antenna at 600MHz



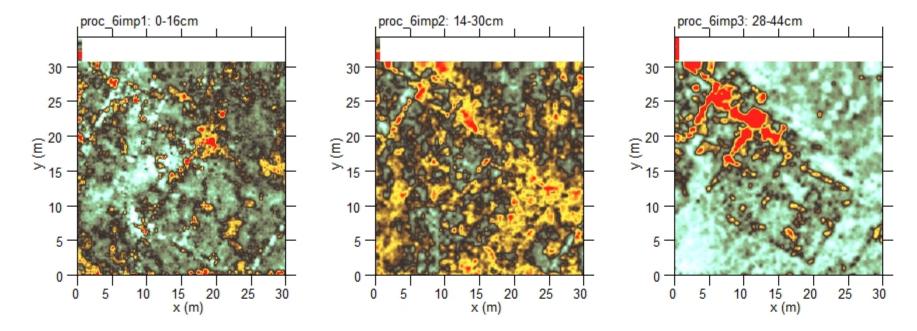
High frequency antenna of the prototype

Egnatia: Pulsed system, antennas at 600 MHz

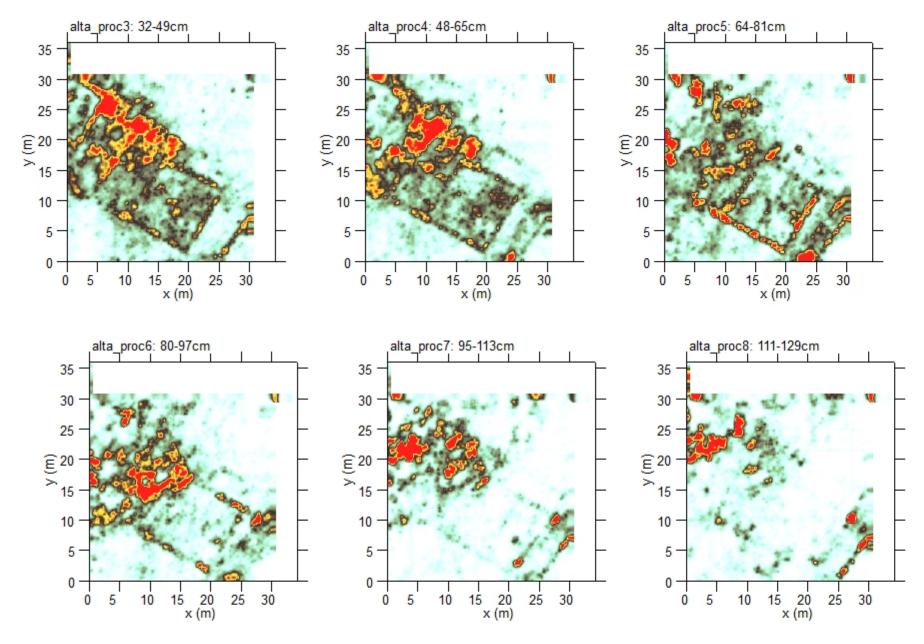


Egnatia: Pulsed system, antennas at 200 MHz

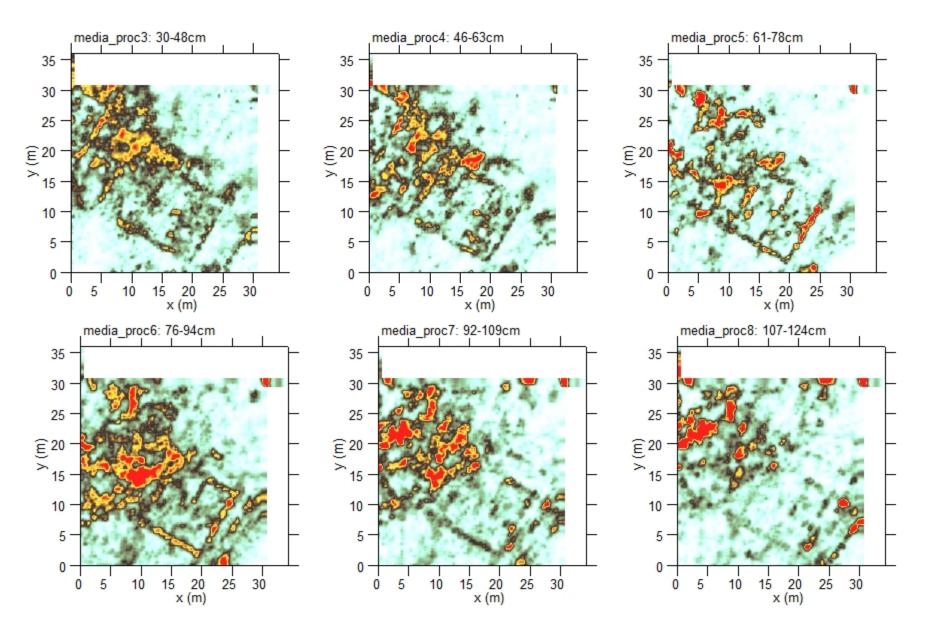
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Egnatia: Prototype, high frequency antennas

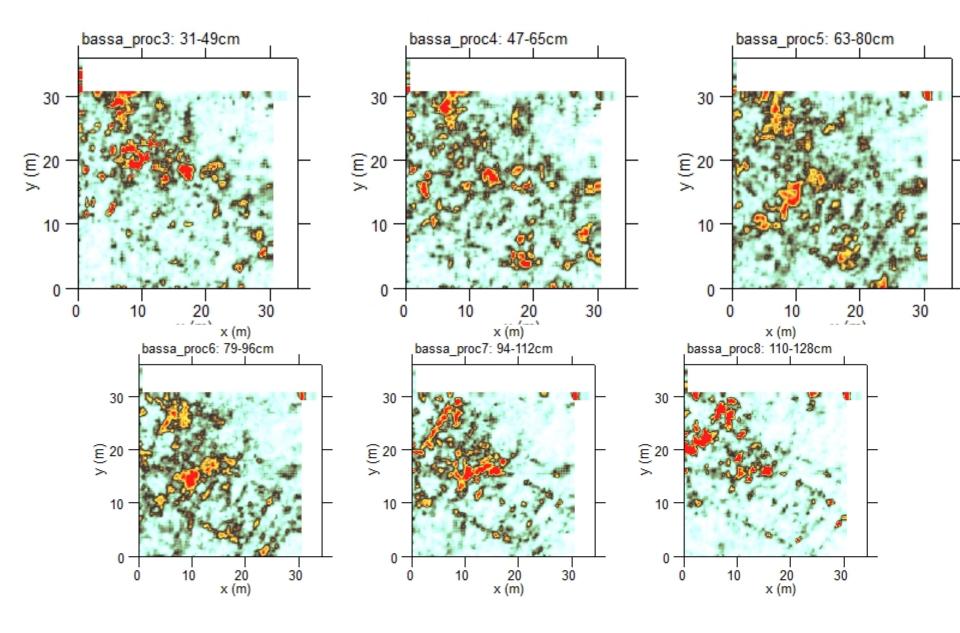


Egnatia: Prototype, medium freq antennas



(m) V

Egnatia: Prototype, low freq antennas



References

[1] R. Persico, D. Dei, F. Parrini, L. Matera, Mitigation of narrow band interferences by means of a reconfigurable stepped frequency GPR system, *Radio Science* 51.8 (2016): 1322-1331.

[2] R. Persico, G. Leucci, Interference Mitigation Achieved with a Reconfigurable Stepped Frequency GPR System, *Remote Sens.* 2016, *8*(11), 926; doi: 10.3390/rs8110926

